### **INFORMATION TO USERS**

The most advanced technology has been used to photograph and reproduce this manuscript from the microfilm master. UMI films the text directly from the original or copy submitted. Thus, some thesis and dissertation copies are in typeswriter face, while others may be from any type of computer printer.

The quality of this reproduction is dependent upon the quality of the copy submitted. Broken or indistinct print, colored or poor quality illustrations and photographs, print bleedthrough, substandard margins, and improper alignment can adversely affect reproduction.

In the unlikely event that the author did not send UMI a complete manuscript and there are missing pages, these will be noted. Also, if unauthorized copyright material had to be removed, a note will indicate the deletion.

Oversize materials (e.g., maps, drawings, charts) are reproduced by sectioning the original, beginning at the upper left-hand corner and continuing from left to right in equal sections with small overlaps. Each original is also photographed in one exposure and is included in reduced form at the back of the book.

Photographs included in the original manuscript have been reproduced xerographically in this copy. Higher quality 6" x 9" black and white photographic prints are available for any photographs or illustrations appearing in this copy for an additional charge. Contact UMI directly to order.

UMI

University Microfilms International
A Bell & Howell Information Company
300 North Zeeb Road. Ann Arbor, MI 48106-1346 USA
313/761-4700 800/521-0600

## Order Number 1\$41568

Later aftershocks of the March 2, 1987 Edgecumbe, New Zealand, earthquake

Zhang, Jianjun, M.S. University of Nevada, Reno, 1990



## University of Nevada-Reno

#### Later Aftershocks of the March 2,1987 Edgecumbe, New Zealand, Earthquake

A Thesis submitted in partial fulfillment of the requirements for the degree of Master of Science in Geophysics

BY

JIANJUN ZHANG

May 1990

The thesis of Jianjun Zhang is approved:

J. G. Anderson

Jamis M Brune

R. hmai

Department Chairman

Graduate Dean

University of Nevada-Reno

May 1990

#### Acknowledgement

The author of this thesis wishes first to thank Dr. John Anderson for his precious academic advice on the study in this thesis and for his various kind support during the study. This study would be impossible without his support.

The author of this thesis also thanks Dr. James N. Brune and Dr. R. Siddharthan for their willingness to participate in the graduate committee. Specially the author thanks Dr. James N. Brune for the financial support in the course of the study.

Finally thanks go to Geoffrey King and Keith Priestley for their generously providing data to this study. The author very much appreciates the discussion with Dr. William Peppin and thanks him for providing help on computer facilities.

This research was completed with partial support from the State of Nevada Nuclear Waste Project Office.

# Later Aftershocks of the March 2, 1987 Edgecumbe, New Zealand, Earthquake

#### ABSTRACT

The March 2, 1987 Edgecumbe, New Zealand earthquake had a magnitude ( $M_L$ ) 6.3 and seismic moment  $7.0*10^{18}$  N\*m. Later aftershocks, from March 15 to 27, were monitored with 10 portable smoked paper recorders operated by the United States Geological Survey, and by seven digital event recorders from the University of Nevada, Reno. Two magnitude scales for these aftershocks were established by calibration of amplitudes and coda durations with seismic moments determined from digital records for 18 events. Most events analyzed have magnitudes between 1.0 and 2.8.

Aftershocks form a zone at least 50 km long striking about N40°E. In the southwestern part, the epicenters are in a narrow zone (<7 km) which broadens to over 15 km wide in the northeast. The depth distribution peaks at 6 km, and most of the events are between 3 and 11 km. A gap in the epicenter distribution near Mt. Edgecumbe suggests the high temperature in that area. Both the depth distribution and epicenter distribution are consistent with the geology of the region: the area has a thin crust and high heat

flow which is a consequence of back arc spreading.

Focal mechanisms indicate predominantly normal faulting with a small strike slip component. Fault strikes are consistent with the trend of the epicenter distribution, with an extension axis which is about N145°E. The preferred fault planes are often ambiguous, but when combined with geological data they are consistent with a dip angle 50 degree downthrown northwest in the northern part of rupture. In the southern part, a southeasterly dip may be preferable. Some mechanisms which deviate from this trend imply the geological complexity in the region.

## Table of Contents

Title pagei
Signature pageii
Acknowledgementiii
Abstractiv
Table of contentsvi
Table of figure and table captionsvii
INTRODUCTION
GEOLOGICAL SETTING5
DATA COLLECTION9
HYPOCENTER LOCATIONS
FOCAL MECHANISM ANALYSIS22
CONCLUSION35
REFERENCES50

# Table of Figure and Table Captions

# Figure Captions:

Figure	1		Major surface ruptures in 1987					
			Edgecumbe earthquake and					
			Rangitaiki Plain2					
Figure	2		Central Volcanic Zone and					
			North Island Shear Belt6					
Figure	3		Station sites and later					
			aftershock epicenters (Mar.15-27)11					
Figure	4	(a-1	n) Aftershock epicenters day by day					
from Mar.15 to Mar.2719-31								
Figure	5a		Cross section distribution along AA'36					
Figure	5b		Cross section distribution along BB'37					
Figure	5c		Cross section distribution along CC'38					
Figure	5d		Cross section distribution along DD'39					
Figure	6a		Coda duration magnitude vs moment					
			and moment magnitude40					
Figure	6b		Amplitude magnitude vs					
			coda duration magnitude41					
Figure	7		Magnitude vs time42					
Figure	8		Histogram (Mar.15-27)43					
Figure	9		Focal Mechanism of four					
			aftershock clusters48					

# Table Captions:

Table 1	Velocity model used in						
	hypocenter locating14						
Table 2	Aftershock event list15-18						

#### INTRODUCTION

The March 2, 1987 Edgecumbe earthquake occurred near the northeastern shore of the North Island of New Zealand. The main shock had magnitude M<sub>1</sub> 6.3, seismic moment  $M_0 = 7*10^{18}$  N\*m [Priestley 1989], and focal depth 8 Km for the main shock [Anderson and Webb 1989]. The focal mechanism based on body waves indicated predominantly normal faulting (Staff of New Zealand Department of Scientific and Industrial Research 1987, Anderson & Webb 1989). But normal mode analysis indicated an important strike slip component was also present (Priestley 1989). The observed surface ruptures after the earthquake also revealed both normal and strike slip components (Geoffrey King 1989, personal communication, Beanland at al 1989). The maximum vertical offset on the ground surface due to the main shock was measured as 2.5 m and the average was 1.4 m on the Edgecumbe fault. An eyewitness saw the rupture propagating from northwest to southeast on the Edgecumbe fault during the main shock [Beanland at al 1989]. Soon after the earthquake a systematic field survey was carried out by the Department of Scientific and Industrial Research, New Zealand, as well as other geological institution like United States Geological Survey. More than 10 surface ruptures due to this earthquake were observed (Figure 1). Some ruptures occurred on pre-existing but previously unrecognized fault scarps, while some others were new surface breaks. Most of the observed surface ruptures had a strike trending northeast

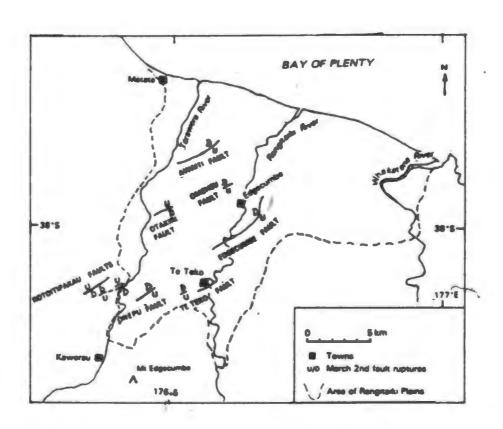


Fig.1 - Onior familto, surface reposes and Rangitaiki Plain.
(suffer formitted at al 1989)

N

downthrown to the northwest, while a small number of ruptures were downthrown to the southeast (Fig 1). The longest rupture was 7 km and the shortest 0.5 km. The pre-existing Edgecumbe fault trace had the most significant surface rupture.

The Edgecumbe earthquake occurred in the Whakatane Graben which is at the northeast corner of Central Volcanic Region. The Central Volcanic Zone extends from the central part of the North Island north to the ocean. This extensional region has been explained as the on-land expression of a young oceanic back arc basin which extends to the north behind the Kermadec subduction zone (Stern 1985). The zone has a high heat flow, and mostly shallow earthquakes, but also some deeper events on the subduction zone. All historical earthquakes in this region have had magnitudes less than 7. The corresponding segment of the Kermadec subduction zone, east to the Central Volcanic Zone, experienced a magnitude 8 earthquake in 1931 (Hawkes Bay earthquake). The Central Volcanic Zone has large, normal faults on both its eastern and western boundaries. Most of the recent seismic activity in the Central Volcanic zone has not involved these faults, and has mostly been associated with volcanic events. The Edgecumbe earthquake neither involved faulting on the main boundary faults, nor was it closely associated with volcanic activity. Rather the surface expression primarily involved smaller faults central to the Whakatane graben.

The Edgecumbe earthquake was perhaps the most significant earthquake in New Zealand in the past two decades. There was extensive damage in the towns of Edgecumbe and Te Teko, and an

important set of strong motion accelerograms was obtained. The earthquake provided an opportunity to study the expression of a back arc system on land.

After the main shock on Mar 2, portable seismic recorders were installed and operated by seismologists from Department of Scientific and Industrial Research, Wellington, New Zealand, from the Seismological Laboratory, University of Nevada-Reno and from the United States Geological Survey, Golden, Colorado. In this paper we study the later aftershock data (from Mar 15 to Mar 27) primarily as recorded on ten portable smoked drum recorders operated by USGS, and supplemented by records from seven digital recorders operated by the University of Nevada-Reno, to investigate the rupture properties and the focal mechanism of the source.

New Zealand is on the boundary between the Pacific and Indian plates. Along the eastern coast of North Island the Pacific plate is thrusting under the Indian plate. Two major tectonic features of North Island are North Island Shear Belts and the Central Volcanic Zone (Figure 2). The shear belt strikes south-north across North Island. It consists of several active light-lateral strikeslip faults with relatively small reverse components. quantitative slip rate was estimated as 14 mm/year of strike slip and 4 mm/year of reverse slip [Sisson 1979, Nairn & Beanland 1989]. The northern end of the shear belt intersects the northeastern part of Central Volcanic Zone at the Whakatane graben where the 1987 Edgecumbe earthquake occurred. The severe 1866 earthquake, which was the last strong earthquake before the 1987 Edgecumbe earthquake in the Whakatane graben, was suspiciously related to one of major faults of the belts but the earthquake was only described in a story and lacked data to make it fully explained [Nairn & Beanland 1989].

The other important feature of north island is the Central Volcanic Zone (CVZ). This region is shaped like a sector with origin at heart of the island and diverging to north. It is an extensional environment with extremely high heat flow (about 700-800 mW/m² [Studt & Thompson 1969]). The CVZ consists of a huge volume of Quaternary rhyolitic volcanic rocks (estimated as about 12,000 km³ [Cole 1979]). The CVZ was explained as a back arc

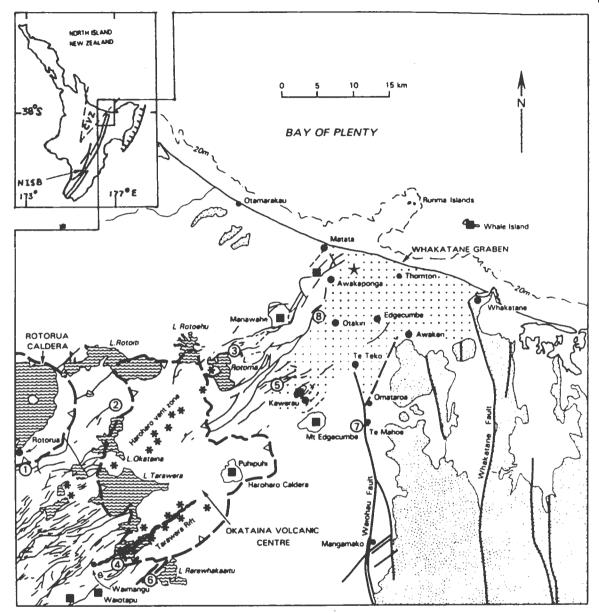


Fig.2 - Central Volcanic Zone and North Island Shear Belts. (after Nairn & Beanland 1989)

Tectonic map of the Bey of Plenty region showing relationships of Whekatane Griben, Olutaina Volcanic Centre, and fault traces of the Taupo Fault Belt and North Diand Shear Belt. Syntholo as for Fig. 1.1 Horohoro Fault; 2 Whakapoungakau Fault; 3 North Roloma Fault; 4 Rotomahana Fault; 5 Rotoitipakau Fault Zone; 6 Rerewhakaaitu fissures; 7 Malahinu Dam; 8 Braemar Fault Faults shown within Whakatane Graben are pre-1987 traces.

spreading center behind the Kermadec trench along the east coast and was recognized as the continuation of a subsidence trough right off coast in the Bay of Plenty [Stern 1978]. The average crust thickness in CVZ is only about 15 km [Stern 1985]. Of more tectonic significance is the eastern part of the CVZ, called Taupo Volcanic Zone (TVZ) which contains numerous active small faults and recent volcanism. In some places in the TVZ, for example Tarawera and Waimangu, one finds the eruption of basalt, with origin in the mantle. Thus one might expect faults dominated by near vertical and dike eruption fractures. But the intrusive volcanic vents do not correspond to the observed fault traces. Furthermore, many faults have a dip angle of 45°-55°, and can only be explained as the result of normal faulting instead of dike eruption. From the investigation of pyroclastic deposits which were already dated [Nairn 1976], it is concluded that most of the faults in northern TVZ had repeated displacements in the recent 50,000 years. The last significant displacement occurred about 1850 years ago by indication of the Taupo pumice deposit.

The 1987 Edgecumbe earthquake occurred in the Whakatane graben. Whakatane graben is at the northern end of TVZ. In the 20 km wide graben, the greywacke basement subsided 2 km below sea level by the interpretation of gravity contours [Nairn & Beanland 1989]. The graben is filled with volcanic ashes and marine deposits of Holocene sediments which formed todays Rangitaiki Plain. Geodetic surveys covering the northern part of TVZ gave a spreading rate of 7 mm/year [Sisson 1979, Nairn & Beanland 1989]. Most of

this spreading was contributed by the TVZ normal faults within the Whakatane graben. From geothermal drillholes, an estimation of the average subsidence rate of the Whakatane graben is around 1 mm/year. Close to the graben axis it reached 2-3 mm/year during past 5500 years (Pullar 1981, Nairn & Beanland 1989). While the graben was subsiding and was extending horizontally its margin was uplifting. The marine sediments with age of 120,000 years at the eastern margin and the Matahina ignimbrite with age of 290,000 years were uplift about 60 m and 300 m respectively; they are considered to have been deposited at the same level as today's sea level. So, from comparing Quaternary marine sediments or the Matahina ignimbrites obtained from geothermal drillholes the uplift of graben margins was estimated as 0.5 mm/year for eastern margins and more than 1 mm/year for western margins [Nairn & Beanland 1989]. The mechanism of uplift in such an extensional graben environment was likely explained by the intrusion of magma underneath, but it is still not certain [Nairn & Beanland 1989].

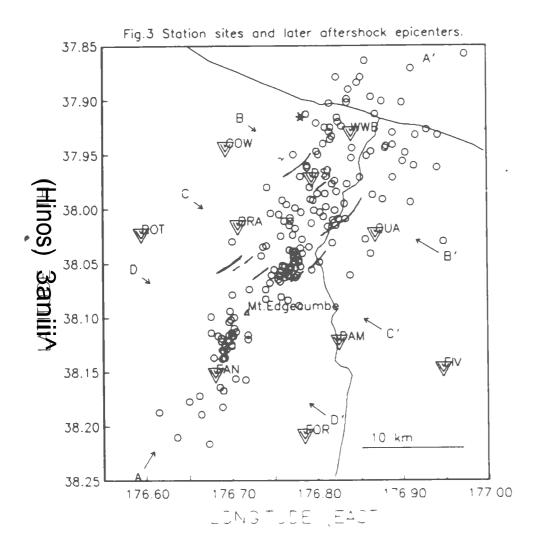
The 1987 Edgecume earthquake was the continuation of the process of Whakatane graben subsiding and extending. This process has been going on since Mid-Quaternary period. It is generally recognized that the Edgecumbe fault within the graben played a major role in the 1987 Edgecumbe event. Study of the Taupo Pumice deposit at the Edgecumbe fault indicated two major events within the last 1850 years; one was about 800 years ago [Nairn & Beanland 1989, Beanland at al 1989]. They suggest that the major earthquake cycle on the Edgecumbe fault would be near 1000 years.

#### DATA COLLECTION

Ten portable smoked paper recorders were distributed as in figure 3. All of these recorders were short period vertical seismometers and worked with a paper speed of 1 mm per second. The clock calibration was read every time recording paper was changed (about 48 hours per sheet of recording paper). Typically the clock drift is about 20 - 40 millisecond per 48 hours. Those clock calibrations were taken into account by linear interpolation for aftershock locating. On average, each located event was effectively recorded by 4 to 8 stations. Major factors which prevented more complete recording included trace obscured by larger events, small amplitudes caused by far distance between event and station, and occasional mechanical problems of recorders. As many aftershock events were picked as possible but many of these events could not located unambiguously.

In order to increase record reading resolution a microscope with a magnifying power 20 was used to read the smoked paper records. The resolution with such a microscope can easily reach 0.025 mm. Since every millimeter on the recording paper represented 1 second that resolution means reading accuracy of 25 millisecond was achieved. P arrivals were usually very obvious and can generally be picked up with the above accuracy. S arrivals were of course often difficult or ambiguous to identify, and in many cases they were not identified at all. Also read at the same time was the first arrival polarity Up or Down of the event, for focal

mechanism analysis. Two parameters were read for magnitude estimation: the peak to peak amplitude and the signal duration. Both were read by a digital caliper and the reading accuracy was about 0.5 millimeter.



The program HYPOINVERSE [Klein 1978], which uses an inversion method via singular value decomposition, was used to locate all the aftershocks in our study. Only events with relatively reliable locations, which had a vertical uncertainty (in sense of one standard deviation) less than 5 km and had at least 4 stations participated effectively in locating, were used in our analysis. The velocity model was the same Edgecumbe model as used by Robinson in his study of early aftershock locations [Robinson 1989], and is listed in Table 1. This velocity model was derived using 38 wellrecorded events with a method that estimated hypocenters and velocity model simultaneously [Crosson 1976]. All the epicenter locations are shown in Figure 3. The mark (\*) is the main shock. Table 2 lists all later aftershocks we located, where ORIGIN is the event origin time (year-month-day-hour-minute and second); LAT and LON are the latitude (°S) and longitude (°E) of located epicenter; DEPTH is focal depth; RMS is root of mean weighted squared error of residual between observed and calculated arrival time in second; ERH and ERZ are horizontal and vertical uncertainty under one standard deviation; GAP is the largest sector in degree that stations didn't cover in locating and the smaller the GAP the better the location; Ma and Mc are amplitude and coda duration magnitude and finally the ESN is the effective station number under which the first digit means the effective stations used in locating and the digit after letter S means how many S arrivals are

effectively used in locating, which could affect the reliability of deep hypocenter locations. Usually in our case horizontal uncertainties are about the same size as vertical uncertainties.

Taible 1 (Wedlocity Model)

Depth	(km)	P	Vedlocity	(km//sec)
0.0	= 1.0		2.40	
1.0	- 6.0		5.00	
6.0	- 10.0		5.91	
10.0	- 15.0		6.55	
15.0	_		7.50	

Table 2 (Aftershock Event List)

			m	* * * * * * * * * * * * * * * * * * * *	TON B	DEDMII	DMC	ERH	מחמ	CAD	Wa	Ma	ESN
		IGIN YMDI			LON E	DEPTH				GAP		Mc	
_	87	3150029			176.811	4.2	.08	1.6				2.3	
_	87	3150239				14.6	.20	2.9				1.9	
3	_	3151730			177.014	16.1	.00	2.1		289		1.9	
4	-	3160843				4.5	.00	. 1	. 2		2.1	2.4	
5	_		13.27		176.810	8.9	. 24	1.5	3.9	124		2.3	
6	87	3161813				13.2	. 14	1.9	. 7		2.5		
7		3161852			176.835	12.2	. 22	1.5	2.5			2.1	
8	87	3170040			176.765	4.5	.00	. 4	. 2	237			
9		3170042			176.789	4.3	.03	. 2	. 3			2.5	
10	87	3170103				9.7	.12	3.1		208		1.9	
11	_	3170137				6.4		3.1		341		2.0	
12	87	3170359				3.9	.26	1.2				2.3	
13	87	3170449				5.2		11.8		231		1.7	
14	87	3170550			176.789	3.8	.04	. 2		126			<b>6</b> S0
15	87	3170629				4.6	.12	2.9	. 8			2.0	
16	87	3171103	12.59	37.992	176.796	4.0	.27	. 7	1.7			2.2	
17	87	3171115	23.47	37.899	176.835	6.4	.31	8.3	3.9	271	2.4		<b>7S</b> 0
18	87	3171412			176.747	. 0	.08	. 3		138			<b>4</b> S1
19	87	3171619	26.00	37.960	176.914	6.1	.13	1.7		232		1.9	
20	87	3172028	6.50	38.034	176.741	5.4	.28	1.2	1.6	109	1.9	1.9	6S0
21	87	3172226	53.80	37.950	176.802	4.6	.04	. 5	. 3	228	1.7	1.8	5S0
22	87	3180123	16.99	38.119	176.688	. 0	.17	. 9	1.1	186	2.2	2.0	5S1
23	87	3180301	12.71	37.953	176.840	7.1	.05	1.2	1.8	247	2.2	2.5	5S0
24	87	3180718	59.03	38.024	176.772	7.2	.09	. 4	1.0	125	1.9	1.7	6S1
25	87	3180957	24.72	38.035	176.791	5.5	.41	2.5	2.6	94	1.8	2.0	<b>6</b> S0
26	87	3181105	30.03	37.864	176.856	9.7	.08	1.6	. 5	286	2.2	1.8	5S1
27			15.28	38.030	176.948	3.8	.00	. 4	. 2	245	1.9	2.3	<b>4</b> S0
28	87	3181444	1		176.862	4.8	.95	6.5	4.6	134	1.7	1.8	6S1
29	87				176.808	7.5	.05	. 5	1.0	160	1.8	1.7	5 <b>S</b> 0
30	87	3181718				9.4	.07	2.7	. 5	285	2.3	1.9	6 <b>S</b> 0
31	87	3181812				7.0	.04	. 5	5.0	171	1.7	1.6	<b>4</b> S0
32	87	3181949				7.4	.01	. 2	. 7	204	2.2	2.1	5S0
3 3		3182153				7.1	.06	1.6	3.4	276	2.5	2.2	6S0
34		3182222			176.810	9.4	.03	. 7	. 4	254	2.2	2.2	5S0
35		3190452				7.3	. 05	1.2	2.0	261	2.3	2.5	6S0
	87	3190608			176.764	5.7	.08	. 4	. 4	113	1.8	1.8	6S0
37		3190634			176.719	7.8	.02	. 2	. 8	167	2.0	1.8	4S1
38		3190723			176.760	16.3	. 02	2.3	2.6	227	2.0	1.8	<b>4</b> S0
39	-	3190848				10.1	.02	. 5	.7	210	1.8	1.6	4S1
40	_	3190907			176.760	6.3	.07	. 3				1.9	
-		3191107				5.0	.10	. 7				1.8	
		3191324				6.9	.00	. 2				1.7	
		3191415				5.7	.06	1.2				1.7	
		3191456				4.6	.05	. 2				2.2	
		3191656				6.4	.06	. 3				1.8	
		3191838					.03	2.5				1.6	
		3192008				7.1	.00	.3				1.8	
		3192240				8.5	.13	. 6				1.9	

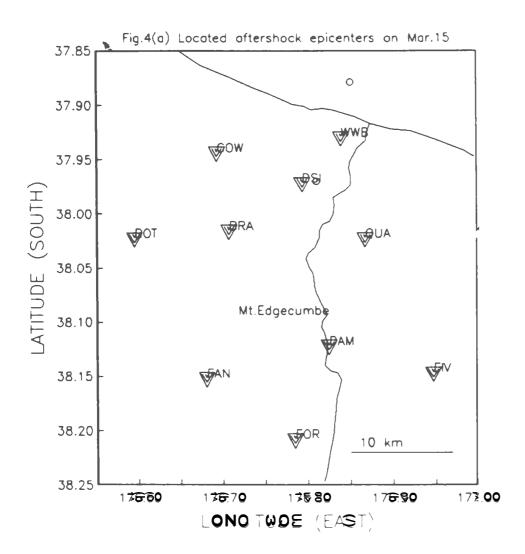
-

```
ERZ GAP Ma
                                                                     Mc
                                                                         ESN
No. ORIGIN YMDHM Sec
                      LAT S
                              LON E
                                       DEPTH RMS
                                                   ERH
                                                         .4 124 2.1 1.9 4SO
                                              .01
                                                    . 3
 49 87 3200605 27.56 38.131 176.691
                                        7.7
                                                    . 3
                                                        2.8 150 2.0 2.2 6SO
                                              .07
                 8.29 38.089 176.779
                                        2.2
 50 87 3200824
                                                         .4 120 2.3 2.1 5SO
 51 87 3201313 50.45 38.129 176.694
                                        7.9
                                             .02
                                                    . 2
                                                        1.5 114 1.7 1.8 4S1
                 4.42 38.137 176.692
                                        7.8
                                             .11
                                                   1.0
 52 87 3201315
                 7.62 38.100 176.703
                                                    . 4
                                                        1.4 114 1.9 1.9 5SO
                                        6.3
                                             .07
    87
       3201504
                                                         .4 259 2.1 1.8 4S2
       3201520 22.97 38.216 176.673
                                        5.6
                                                    . 9
                                             .07
                                                         .2 188 2.2 2.0 5SO
 55 87 3201559 26.07 38.127 176.692
                                        5.6
                                              .03
                                                    . 3
                                                         .8 128 2.3 2.2 6S1
                                                    . 4
 56 87 3201653 54.07 38.130 176.689
                                        7.5
                                              .06
                                                         .2 134 2.2 2.2 6SO
                                                    . 2
                                        5.2
                                              .03
 57 87 3201737 47.49 38.122 176.688
                                                         .4 299 2.4 2.0 5SO
 58 87 3202330 13.56 37.903 176.815
                                                   2.2
                                        9.6
                                              .01
                                                    . 2
                                                         .7 131 2.0 1.8 6SO
       3210451 39.50 38.045 176.773
                                             .03
                                        7.8
 59 87
                                                        1.0 115 2.0 1.8 6SO
       3210656 14.70 38.055 176.768
                                              .04
                                                    . 2
                                        8.1
 60 87
                                                         .7 267 2.3 2.2 7SO
 61 87
       3210758 28.72 37.971 176.889
                                        6.6
                                              .06
                                                   1.1
                                                         .4 278 2.4 2.1 751
 62 87 3210834 48.67 37.930 176.889
                                        8.7
                                              .06
                                                   1.3
                                                    . 9
                                        7.4
                                              .06
                                                        1.9 129 2.0 1.9 5SO
 63 87 3210929 14.89 38.035 176.737
                                                         .6 110 2.1 2.0 7SO
                                              .03
                                                    . 1
 64 87 3211459 28.54 38.057 176.758
                                        6.6
                                                    . 2
                                                        1.6 118 2.1 2.2 7SO
 65 87 3211820 25.50 38.094 176.698
                                        3.9
                                              .05
                                                        3.2 112 2.4 2.3 7SO
                                                    .8
                                        9.2
                                              .18
       3211825 50.15 38.079 176.701
 66 87
                                                         .2 206 1.8 2.0 6S0
                                              .05
                                        5.8
                                                    . 6
 67
    87
       3211929 56.83 38.003 176.804
 68 87 3211946 43.39 37.942 176.881
                                                        1.7 274 2.3 2.2 7SO
                                        6.3
                                              .05
                                                   1.3
                                                        1.4 240 2.0 1.9 5S2
                                                    . 7
 69 87 3211947 45.23 37.940 176.808
                                        7.7
                                              .09
                                                          .3 119 1.8 1.7 5S1
                                              .05
                                                    . 2
 70 87 3212212 23.65 38.065 176.755
                                        5.9
                                                         .2 104 2.0 2.0 7SO
                                                    . 2
 71 87 3212308 47.73 38.061 176.757
                                        5.8
                                              .05
                                              .28
                                                             96 1.7 1.8 5S1
 72 87 3212317 55.87 38.074 176.721
                                                        1.8
                                        5.6
                                                   1.6
                                              .00
                                                         .4 239 1.6 1.5 4S0
                7.41 38.084 176.766
                                                    . 3
                                        6.2
 73 87
       3220802
                                                        4.9 201 2.0 1.6 5S1
       3221151 30.01 38.099 176.676
                                              .24
                                                   1.9
                                       14.4
 74 87
                                                    . 7
                                                         .1 299 1.8 1.7 4S0
 75 87 3221237 43.39 37.994 176.910
                                        4.7
                                              .00
                                                         .3 215 1.5 1.7 4S1
                                              .00
                5.40 37.974 176.821
                                        6.6
                                                    . 2
 76 87 3221528
                                                    .8
                                                        2.8 190 2.3 2.5 8SO
 111 87 3221544 16.52 38.114 176.676
                                        3.2
                                              .10
                                                         .9 138 1.7 1.5 4SO
 718 87 3221744
                3.00 38.053 176.763
                                        5.2
                                              .00
                                                    . 1
                                                         .2 212 1.7 1.8 4SO
                                              .00
                                                    . 2
 79 87 3221750 38.77 38.114 176.700
                                        5.3
                                                         .3 155 1.8 1.7 6SO
                                                    . 3
 80 87 3221812 49.94 38.117 176.702
                                        5.8
                                              .05
                                                         .6 106 2.0 2.1 7S1
 81 87 3222214 12.99 38.062 176.757
                                        5.2
                                              .10
                                                    . 3
 82 87 3222216 44.97 37.986 176.801
                                              .06
                                                    . 7
                                                        1.8 187
                                                                 2.2 2.2 5SO
                                        6.3
                                                         .2 154 1.9 2.0 6SO
                                                    . 3
 83 87 3222252 13.08 38.003 176.782
                                        5.5
                                              .06
                                                             90 1.6 1.9 6S0
                6.70 38.061 176.777
                                        3.3
                                              .06
                                                    . 2
                                                         2.0
 84 87 3230016
                                                         .4 254 2.0 1.7 5S1
                                                    . 3
 85 87 3230023 43.04 37.925 176.816
                                        9.3
                                              .04
                                                          .2 254 2.2 2.1 5SO
 86 87 3230042 45.37 37.956 176.901
                                              .03
                                                    . 8
                                        6.0
                                                          .4 142 1.8 1.9 6S1
                                                    . 5
 87 87 3230125 38.10 38.008 176.769
                                        5.9
                                              .07
 88 87 3230131 24.78 37.962 176.941
                                              .02
                                                    . 3
                                                          .6 284
                                                                 1.9 1.8 4S1
                                        8.3
                                         . 9
                                              .04
                                                    . 2
                                                          .3 138 1.2 1.5 4S1
 89 87 3230224 57.29 38.042 176.777
                                                          .8 109 2.1 2.2 6SO
                                                    . 6
                                              .19
 90 87 3230232 45.23 38.081 176.758
                                        5.6
                                                        2.4 289 2.0 1.7 4S1
                                        8.9
                                              .06
                                                    . 8
 91 87 3230719 16.58 37.884 176.847
                                                          .3 111 2.0 2.1 8S2
                                                    . 4
                8.94 38.126 176.700
                                        5.2
                                              .11
 92 87
       3230803
                                                          .5 125 1.5 1.6 6S2
                                                    . 3
       3231035 48.34 38.083 176.740
                                        5.5
                                              .09
 93 87
                                                          .1 112 1.5 1.7 6SO
                                        5.8
                                              .04
                                                    . 2
 94 87 3231054 50.19 38.125 176.700
                                              .00
                                                    . 2
                                                            125
                                                                 1.5 1.7 4S0
                                        5.7
                                                          . 2
 35 87 3231312 49.69 38.125 176.692
                                                          .9 234 1.9 1.6 5SO
                                              .05
                                                   1.0
 96 87 3231545 52.81 37.995 176.832
                                       10.2
                                                          .3 233 1.6 1.6 4SO
                                              .00
                                                    . 5
 97 87 3231603 23.31 37.971 176.850
                                        8.2
                                                          .7 104 1.5 1.7 6S3
       3231701 36.10 38.063 176.762
                                        5.2
                                              .13
                                                    . 3
 98 87
                                                          .1 114 1.9 1.9 6S1
 99 87 3231818 14.37 38.110 176.703
                                        5.7
                                              .03
                                                    . 1
```

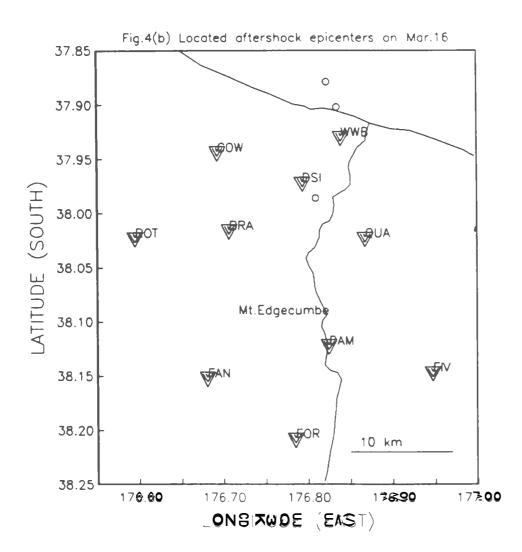
```
No. ORIGIN YMDHM Sec
                       LAT S LON E
                                       DEPTH RMS
                                                   ERH
                                                         ERZ GAP Ma
100 87 3232059 5\overline{4}.75 37.991 176.877
                                         6.4
                                              .11
                                                   1.7
                                                          .8 257 2.2 2.3 5S1
101 87 3232322 32.65 38.056 176.750
                                         9.2
                                              .05
                                                     . 2
                                                          .6 111 1.6 1.6 5S2
102 87 3232338 45.19 37.932 176.942
                                         7.5
                                              .07
                                                   1.4
                                                         1.6 286 2.7 2.3 7SO
       3232345
                 5.50 38.057 176.759
                                         6.4
                                              .10
                                                     . 4
                                                         1.7 110 2.3 2.4 7S1
       3232357 12.23 38.025 176.758
104 87
                                        8.7
                                              .00
                                                     . 4
                                                         1.0 164 1.6 1.6 4SO
       3240011 15.73 38.053 176.760
105 87
                                              .07
                                        8.0
                                                     . 3
                                                          .8 116 1.6 1.7 5S2
106 87 3240014 51.67 38.122 176.697
                                         5.8
                                              .07
                                                     . 3
                                                          .3 160 1.8 1.9 6S1
107 87 3240100 57.24 38.053 176.770
                                         5.8
                                              .08
                                                     . 4
                                                          .6 119 1.3 1.4 481
108 87 3240147 44.88 38.117 176.684
                                        5.4
                                              .13
                                                     . 4
                                                          .5 140 2.3 2.2 7S1
109 87 3240356 48.25 38.074 176.740
                                        2.4
                                                    . 3
                                                         4.7
                                              .11
                                                              83 2.1 2.2 8S1
110 87 3240449 38.34 38.137 176.690
                                        2.3
                                              .06
                                                    . 3
                                                          .9 127 1.5 1.7
                                                                          4S2
111 87
       3240509 42.61 37.889 177.089
                                       14.5
                                              .07
                                                   8.1
                                                         1.1 312 2.2 1.7 5SO
112 87
       3240601 15.73 38.156 176.704
                                          . 8
                                              .08
                                                    . 3
                                                          .3 159 1.6 2.0 6S2
113 87 3240747 27.50 37.839 176.489
                                        2.9
                                              .30
                                                   4.0
                                                         1.4 326 2.0 1.9 6S1
114 87 3240754
                7.94 38.061 176.766
                                                    . 2
                                        4.5
                                              .07
                                                          .8 113 2.1 2.2 8S2
115 87 3240840 10.35 38.068 176.745
                                        5.5
                                              .09
                                                    . 3
                                                          .3 165 1.5 1.6 5S3
116 87 3240845
                  .65 37.948 176.904
                                        8.5
                                              .14
                                                   1.1
                                                          .8 258 2.1 2.1 8S3
117 87 3240846 10.95 37.932 176.916
                                              .21
                                         . 6
                                                   3.1
                                                         1.9 266 1.9 2.0 7S2
118 87 3240903 22.58 38.039 176.772
                                        5.3
                                              .12
                                                    . 5
                                                          .5 109 1.5 1.6 7S2
119 87 3241020 49.25 37.786 176.773
                                        4.8
                                              . 17
                                                  32.3
                                                         4.1 317 1.7 1.9 480
120 87
       3241029 17.60 37.933 176.818
                                        6.0
                                              .20
                                                   1.4
                                                         1.9 249 1.6 1.7 6S3
121 87 3241044 16.37 38.030 176.701
                                              .03
                                                    . 5
                                       14.4
                                                          .7 222 1.4 1.4 4S1
122 87 3241137 17.05 38.122 176.695
                                        9.7
                                              .06
                                                    . 7
                                                          .4 182 1.5 1.6 4S1
123 87 3241206 14.14 37.901 176.876
                                        3.1
                                              .00
                                                   1.2
                                                          .3 297 1.6 1.5 4S0
124 87 3241233 47.45 38.016 176.813
                                        8.2
                                              .09
                                                   1.2
                                                        1.3 186 1.2 1.2 4S1
125 87
       3241250
                2.16 37.765 177.068
                                       10.1
                                              .18
                                                  17.0
                                                        4.2 316 2.5 1.9 750
       3241250 44.37 38.043 176.735
126 87
                                        4.0
                                              .10
                                                    . 4
                                                        1.5 116 1.4 1.6 750
127 87 3241310 33.96 37.977 176.835
                                              .33
                                        6.5
                                                   2.1
                                                        2.5 223 1.4 1.5 5S3
128 87 3241317 46.91 37.951 176.858
                                        4.7
                                                    . 7
                                                         .4 246 1.9 2.0 751
                                              .09
129 87 3241321 12.50 38.049 176.803
                                      13.2
                                              .32
                                                   1.7
                                                        3.4 126 1.4 1.3 4S2
130 87 3241323
                 3.36 37.970 176.781
                                                    . 5
                                        4.9
                                              .05
                                                         .2 235 1.5 1.5 5S2
131 87 3241352 55.72 38.061 176.838
                                        4.7
                                              .04
                                                    . 3
                                                         .3 148 1.7 2.5 481
132 87
       3241418 37.51 37.947 176.863
                                       10.1
                                              .03
                                                   3.6
                                                         .6 270 1.4 1.7 4SO
133 87 3241520 51.93 38.117 176.700
                                        7.5
                                              .00
                                                    . 2
                                                        1.0 176 1.5 1.6 4S0
134 87 3241734 10.11 38.164 176.686
                                        9.9
                                              .12
                                                   1.3
                                                         .9 216 1.6 1.5
                                                                          4S2
135 87 3241802
                 8.96 38.013 176.794
                                        5.4
                                              .03
                                                    . 3
                                                         .1 189 1.4 1.5
                                                                          6S0
136 87 3241818 19.92 38.011 176.769
                                        5.6
                                              .02
                                                    . 2
                                                         .2 191 1.4 1.5
                                                                          4S1
137 87 3241839 58.51 38.009 176.825
                                        8.0
                                              .04
                                                    . 5
                                                         .8 202 1.9 1.8 5S1
138 87 3241902 38.37 37.964 176.813
                                        5.5
                                              .05
                                                    . 6
                                                         .2 251 1.5 1.6 5S2
139 87 3241912 51.71 38.167 176.690 10.0
                                             .13
                                                    . 5
                                                         .5 215 2.0 2.0 6S4
140 87 3242047 21.38 38.038 176.768
                                        5.9
                                             .19
                                                   1.0
                                                         .6 122 2.0 2.0 5S2
141 87 3242319
                 5.37 38.011 176.762 11.2
                                             . 12
                                                        1.2 192 1.9 1.7 4S2
                                                   1.6
142 87 3250501 40.21 38.042 176.773
                                       10.2
                                             .14
                                                    .9
                                                        1.3 122 1.9 1.9 6S1
143 87 3250659 38.53 38.009 176.833
                                                    . 5
                                             .05
                                                         .9 172 1.1 2.0 4S1
                                        2.7
144 87 3250703 37.53 37.929 176.815
                                        8.7
                                             .18
                                                   1.4
                                                        1.0 252 1.4 1.5 7S1
145 87 3250725
                8.62 38.054 176.775
                                        2.6
                                             .08
                                                    . 3
                                                        2.8 130 1.4 1.6 6S1
146 87 3250758 48.84 38.041 176.783
                                        5.5
                                             .06
                                                    . 3
                                                         .3 139 1.3 1.3 5S1
147 87 3250859 40.62 38.001 176.797
                                        7.1
                                             .11
                                                    . 5
                                                        1.1 114 1.4 1.6 751
148 87 3250959 35.13 38.102 176.699
                                        6.6
                                             .02
                                                    . 3
                                                        1.1 212 1.2 1.4 5SO
149 87 3251037 45.11 38.040 176.773
                                        5.9
                                             .07
                                                    . 4
                                                         .4 138 1.4 1.4 5S1
150 87 3251301 58.41 38.036 176.781
                                        5.5
                                             .02
                                                    . 2
                                                         .2 148 1.2 1.6 5SO
```

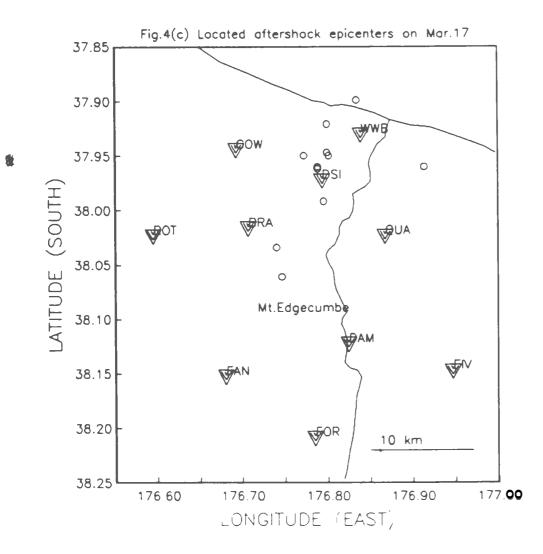
```
No. ORIGIN YMDHM Sec LAT S
                              LON E
                                       DEPTH RMS
                                                   ERH
                                                        ERZ GAP Ma
                                                                     Mc
151 87 3251427 49.86 $7.980 176.792
                                        9.5
                                             .10
                                                         .5 114 1.2 1.2 5SO
                                                   1.0
152 87 3251522
                 5.32 38.001 176.821
                                      12.3
                                             .10
                                                    . 9
                                                        1.6 181 1.8 1.7 550
153 87 3251639 36.92 37.977 176.818
                                             .14
                                                        1.4 208 2.0 2.4 750
                                        6.7
                                                   1.3
154 87 3251640 49.88 37.913 176.788
                                             .00
                                        4.0
                                                   1.0
                                                         .2 297 1.5 1.3 450
155 87 3251700 13.90 37.944 176.841
                                        8.2
                                             .14
                                                   1.1
                                                        1.4 246 1.6 1.7 7S1
156 87 3251701 31.08 37.913 176.868
                                        2.6
                                             .03
                                                    . 8
                                                         .3 266 1.3 1.9 6SO
157 87 3251750 16.29 37.924 176.829
                                        3.8
                                             .13
                                                    . 8
                                                         .8 257 1.8 2.0 6S1
158 87 3251844 51.70 38.053 176.781
                                        6.0
                                             .05
                                                    . 3
                                                         .3 151 1.4 1.7 481
159 87 3251902 37.00 38.063 176.775
                                        5.6
                                             .10
                                                    . 5
                                                         .3 136 1.8 2.0 6S1
160 87 3251940 31.93 37.902 176.900
                                        3.5
                                                    . 8
                                             .10
                                                         .7 275 2.2 2.3 6S1
161 87 3252028 27.64 38.018 176.775
                                        4.9
                                             .08
                                                    . 6
                                                         .4 178 1.3 1.4 582
162 87 3252143 36.76 38.056 176.794
                                        6.8
                                             .00
                                                         .5 236 1.6 1.6 4SO
                                                    . 3
163 87 3252147
                7.51 37.927 176.929
                                             .04
                                        5.0
                                                  1.9
                                                         .4 292 2.1 1.9 5SO
164 87 3252341 12.63 38.062 176.768
                                        6.2
                                             .00
                                                   . 2
                                                         .7 165 1.0 1.4 450
165 87 3252342
                 3.75 38.056 176.769
                                        6.7
                                             .04
                                                   . 3
                                                        1.3 136 1.1 1.3 5SO
166 87 3260635 37.52 37.858 176.974 12.6
                                             .30
                                                  2.7
                                                        1.7 296 2.1 2.0 683
167 87 3260910
                3.63 38.015 176.822 11.5
                                             .02
                                                  1.8
                                                        2.2 127 1.3 1.4 450
168 87 3261028 51.76 37.871 176.911 13.8
                                             .25
                                                  5.0
                                                       1.3 286 2.5 2.5 8S1
169 87
       3261035 46.73 37.987 176.865
                                       7.6
                                             .24
                                                  1.5
                                                       2.3 231 2.2 2.9 751
170 87 3261142 40.37 38.049 176.773
                                       8.4
                                                   . 6
                                             .12
                                                       1.1 154 1.3 1.5 6S3
171 87 3261153 28.21 37.941 176.889
                                       6.4
                                             .10
                                                  1.1
                                                       2.6 257 1.6 1.4 6S1
172 87 3261243 44.88 38.172 176.662 10.1
                                                       2.8 256 1.8 1.6 6SO
                                             .18
                                                  4.6
173 87 3261354 43.78 38.028 176.783
                                       8.1
                                             .23
                                                  1.0
                                                       2.2 104 1.6 1.5 7S2
174 87 3261404 29.57 38.031 176.818
                                             .11
                                       4.9
                                                  2.6
                                                       2.8 123 1.3 1.5 5S1
175 87 3261504 57.21 38.187 176.615 12.6
                                             .13
                                                  3.9
                                                       2.6 276 2.0 1.6 7SO
176 87 3261721 50.05 38.047 176.779
                                       7.8
                                             .28
                                                  1.2
                                                       3.0 122 1.2 1.4 751
177 87 3270112
                                             .09
                 2.36 37.936 176.816
                                       5.4
                                                   . 7
                                                        .3 248 1.5 1.6 6S1
178 87 3270349
                 7.32 38.028 176.856
                                       6.5
                                             .22
                                                  1.0
                                                       1.1 136 1.5 1.7 783
179 87 3270551 43.50 38.067 176.757
                                       6.7
                                             .13
                                                       1.3
                                                   . 4
                                                             83 1.3 1.6 7S2
180 87 3270630 19.96 38.210 176.636
                                       8.2
                                             .14
                                                  3.4
                                                       2.0 263 2.0 1.8 5SO
181 87 3270701
                3.60 38.138 176.689
                                       9.4
                                             .11
                                                   . 6
                                                       1.0 122 2.0 2.0 8S1
182 87 3270753 38.16 37.835 176.580 11.6
                                             .21
                                                 11.6
                                                       1.6 312 2.0 2.0 9SO
183 87 3270915 44.07 37.991 176.793 12.3
                                             .71
                                                       3.5 116 1.6 1.8 854
                                                  3.6
184 87 3270919 59.32 37.944 176.880
                                       8.5
                                             .12
                                                  1.3
                                                       1.4 276 1.4 1.4 6S1
185 87 3271013 46.53 37.980 176.742
                                       8.0
                                             .04
                                                   . 6
                                                        .3 254 1.4 1.5 452
186 87 3271114 55.94 38.182 176.689
                                       5.1
                                             .10
                                                  1.4
                                                        .4 228 1.6 1.6 5S1
187 87 3271142 31.14 38.157 176.716
                                             .00
                                       9.8
                                                   . 4
                                                        .5 151 1.4 1.6 4SO
       3271208 25.03 38.010 176.819
188 87
                                       8.5
                                             .08
                                                   . 4
                                                        .8 161 1.6 1.6 6S2
189 87 3271706
                4.04 38.189 176.664
                                       4.6
                                             .14
                                                  1.7
                                                        .6 242 2.1 2.3 8SO
190 87 3271754 19.75 38.177 176.650
                                       8.6
                                             .16
                                                  1.0
                                                       1.4 239 2.0 1.9 851
191 87 3272019 22.15 38.049 176.779
                                       6.3
                                             .24
                                                   .6
                                                       4.8 103 1.5 1.6 7S1
192 87 3272148 8.00 38.137 176.679
                                       5.2
                                            .16
                                                  1.2
                                                        .7 201 1.9 2.0 6S1
```

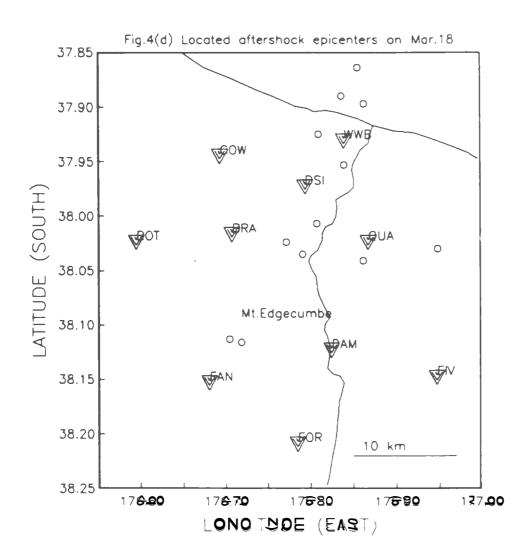
-

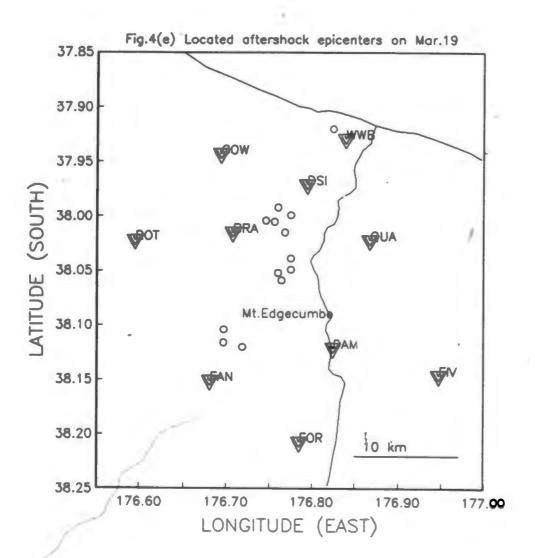


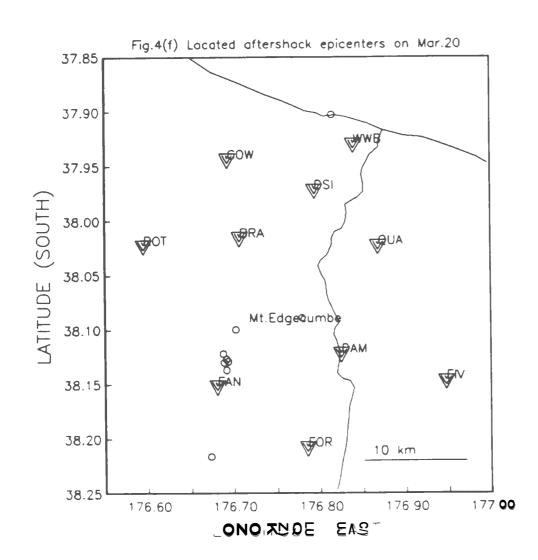
T 🖥

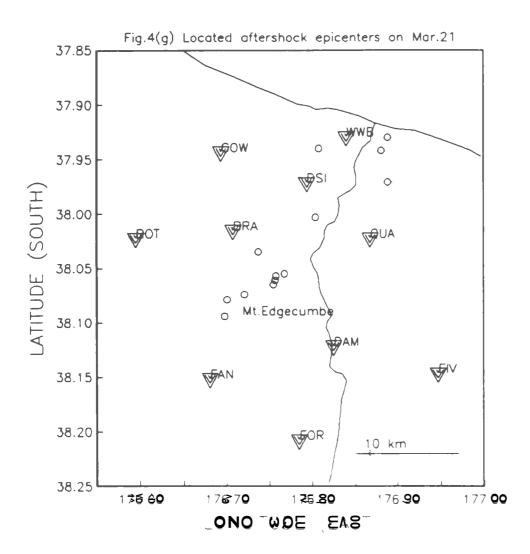


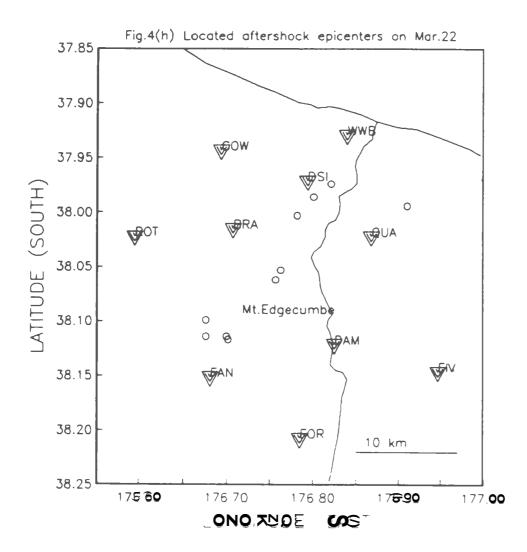


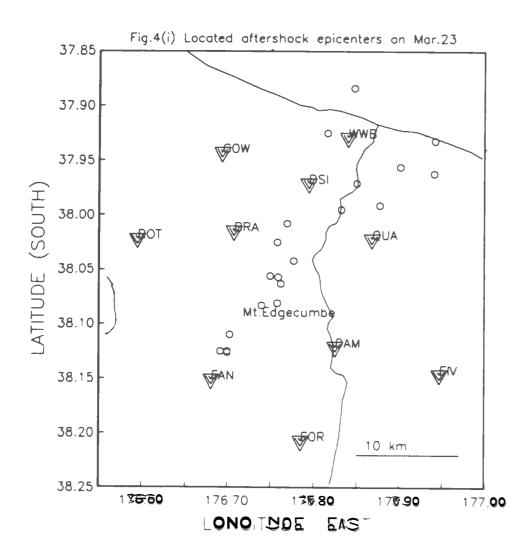


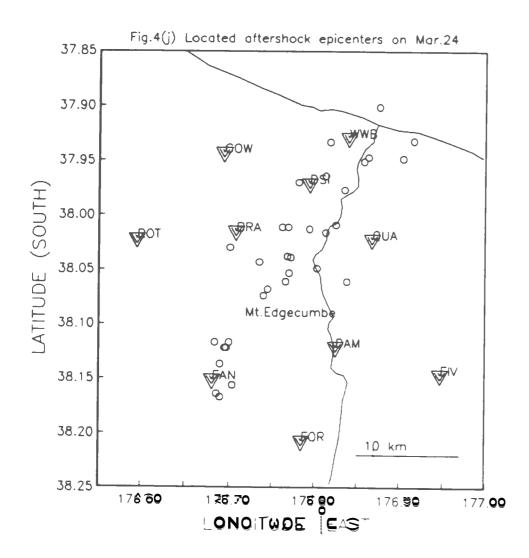


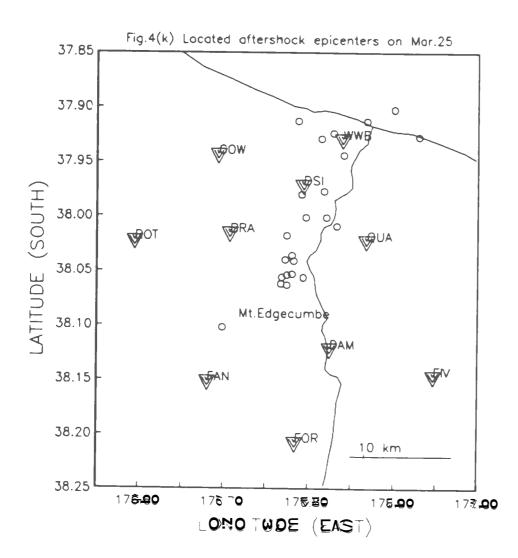


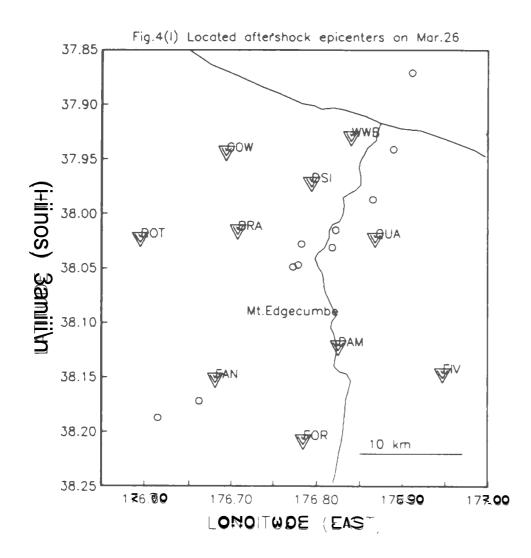




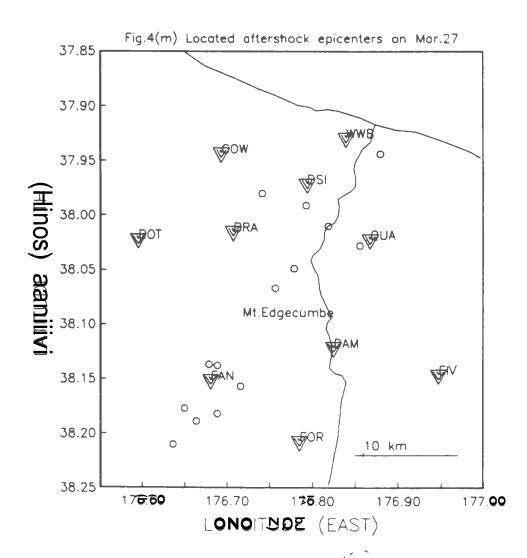








3



بي



Figures 4(a-m) present the aftershocks on each day from Mar.15-27. There are no obvious changes in the pattern of epicenters form day to day.

A least squares fit to the spatial distribution of epicenters shows a N39°E trending direction (AA' in Figure 3). In this direction the later aftershock zone is at least 50 km long. In the southwestern part the epicenters are in a relatively narrow zone (<7 km) and they broaden to over 15 km wide in the northeast. Cross section projections of hypocenters at AA', BB', CC' as well as DD' are given in figure 5a,5b,5c,5d respectively.

On section AA', epicenters are distributed along about 50 km length. There are few epicenters shallower the 3 km, and few located deeper than 12 km. The number of deeper epicenters below Mt. Edgecumbe is decreased relative to other locations along this profile.

Section BB' shows possible subsurface projection of three faults that showed surface rupture after the main shock. The dip, 55 degree, is based on our focal mechanism result as well as previous inference by Nairn and Beanland (1989). The Edgecumbe fault, showing the greatest surface rupture, bisects the aftershock zone. There is no obvious relationship between the hypothesized fault geometry and the aftershock distribution. The later aftershock hypocenters do not define any fault plane, as noticed in the early aftershock study [Robinson 1989].

Mapped surface fault rupture in the region shown on section CC' are much shorter, and no mapped surface faulting occurred in

the region on sectionDD'. Aftershocks in these region are less diffuse. There is a very weak suggestion of a dip to the northwest on section CC' and possibly a dip to the southeast on section DD'. However the trends are also too diffuse to confidently identify possible fault planes.

Most of the aftershocks presented in Table 2 have magnitude from 1.0 to 2.8 and a small number are a little less than 1.0. There are two magnitudes calculated: one from the peak to peak amplitude and the other from coda duration. Magnitude M<sub>c</sub> is assumed proportional to the logarithm of coda duration and parameters are adjusted to be consistent with the moment magnitudes of 18 common events from digital recorders operated by the University of Nevada-Reno. Those moment estimations of the 18 events were derived from spectral analysis of records [Priestley: pers. comm. 1989] and the moment magnitudes were derived from the Kanamori magnitude-moment relationship [Hanks & Kanamori 1979].

The resultant relation we adopted to calculate coda magnitudes in our study is

Coda Magnitude  $M_c = 1.64*log (D_r) - 0.26$ 

where

 $D_r = Duration.$ 

Those events which were recorded on smoke paper and also triggered digital recorders are relatively larger ones. For some

of those events, amplitudes on smoke paper reached saturation. The total common events available are only 18. It is expected that there are big errors, because of the saturation, if we also directly use the moment magnitudes to adjust the parameters in magnitude-peak amplitude relationship. Instead amplitude magnitude is derived through the linear regression with the derived coda duration magnitude.

The resultant relation we adopted to calculate amplitude magnitudes in our study is

Amplitude Magnitude  $M_a \# \log (A_m/2) + 0.8*\log (D_e^2 + D_D^2) -0.6$ 

where

D<sub>e</sub> = Epicenter Distance;

D<sub>n</sub> = Hypocenter Depth;

A = Peak to Peak Amplitude.

The figure 6a and 6b are the fitting lines showing the different magnitudes and the scattering situation.

Both magnitudes so derived are listed in the Table 2 (Event List). The obtained magnitudes of these later aftershocks are obviously smaller than the earlier aftershocks studied by Robinson (1989), most of which are greater than 3.0.

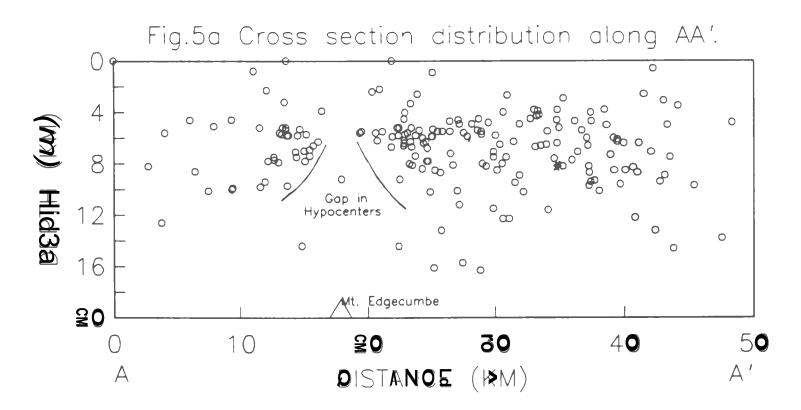
The magnitudes and event times are shown explicitly in Fig.7.

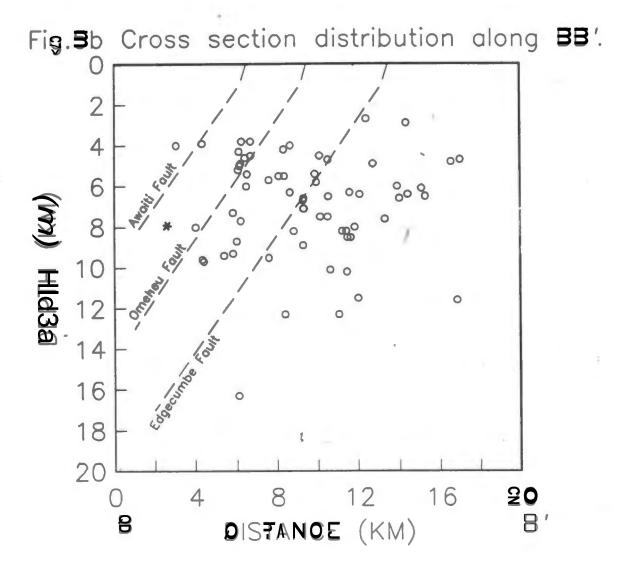
The magnitude of each event in Fig.7 is the maximal one of amplitude and coda magnitudes for the event. The Fig.7 shows that

the completeness of the record of located events compared with time and was at its best between March 23 and 26. For events above magnitude 1.8 there is some suggestion that the number of located events per day is gradually decreasing.

A histogram is given here (Figure 8) which shows most events are within 11 km of depth and aftershock number reaches a maximum near the depth of 6 km. This result is consistent with the main shock location which was estimated at 8 km depth and it agrees with the common situation that rupture usually initiates at the bottom of rupture area of faults for normal faulting [Jackson 1987].

gap between cluster DD' and CC'. The early aftershocks displayed a similar gap in same place [Robinson 1989]. The Holocene Mt. Edgecumbe volcano is in this gap and very high heat flow around that area is expected. The above seismic gap in the aftershock distribution may be caused by the high temperature there, which could prevent accumulation of elastic energy and only allow creep. The cross section along trending direction AA' provided another look of the gap. It seems that focal depth is getting more shallow when getting close to the gap. The events that apparently violate this trend are really projected in the gap from the side. This of course is in another way supporting our suggestion that the gap is due to the high temperatures associated with the volcano.





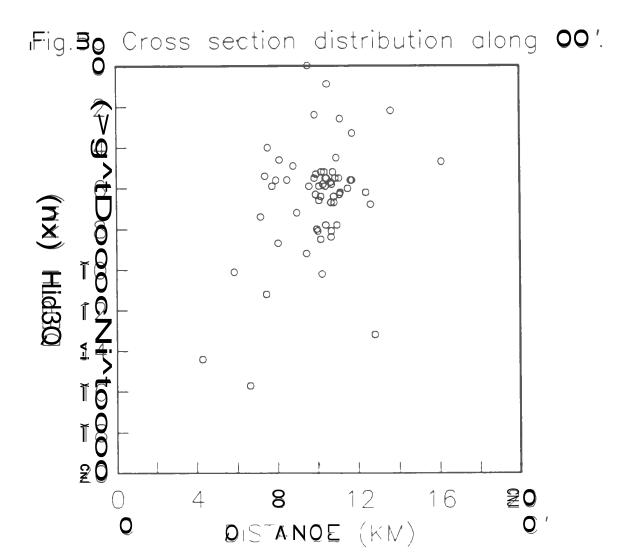
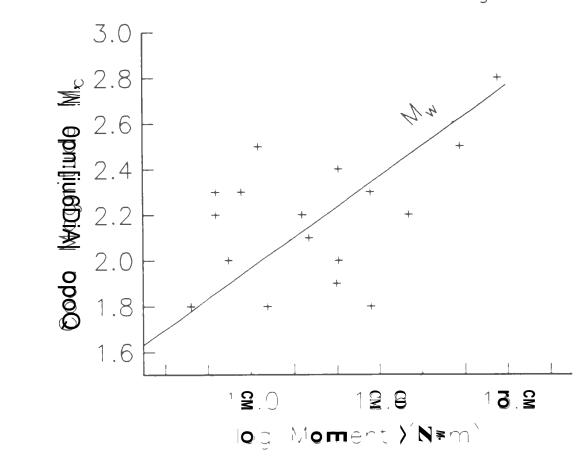
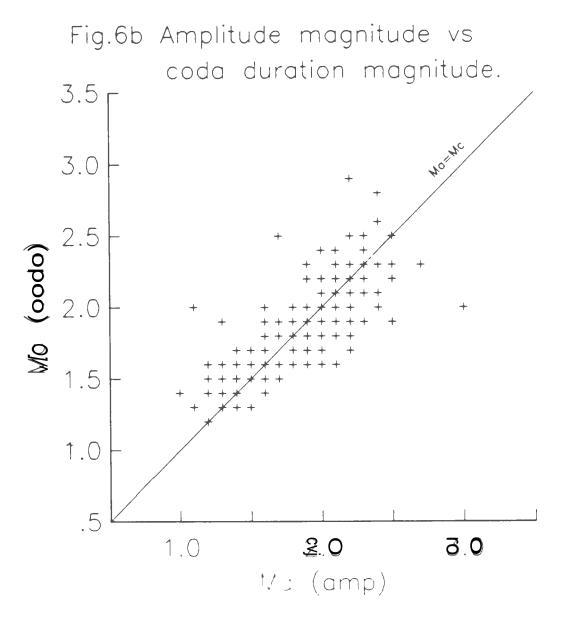
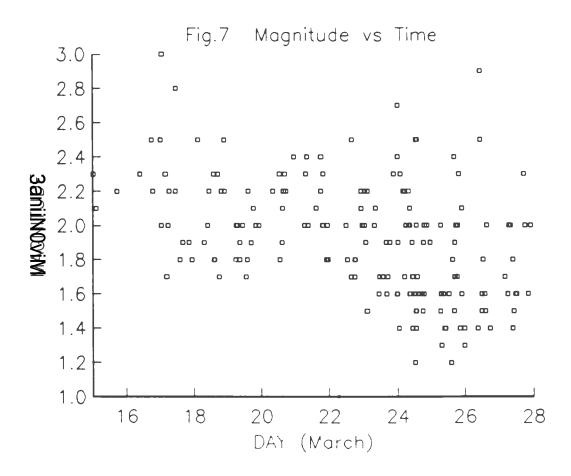


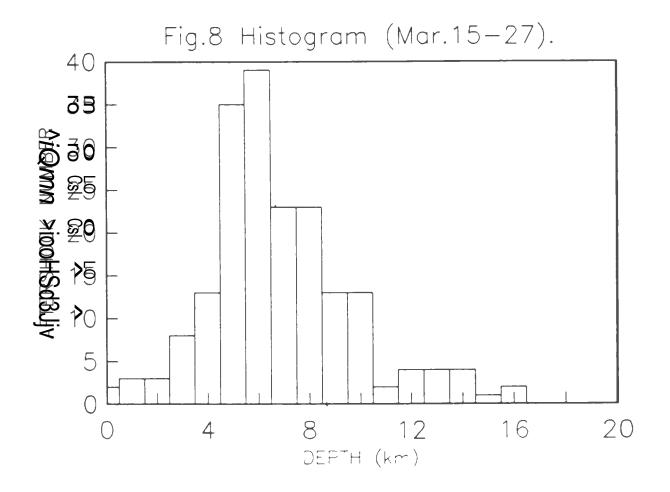
Fig. 3d Cross section distribution along 00'. (M≯i) Hid3a 0' DISTANCE (XM)

Fig.6a Coda duration magnitude vs moment and moment magnitude.









## FOCAL MECHANISM

First arrival polarities (up or down) of all analyzed events were picked for focal mechanism analysis. Results are shown in Fig. 9. The stereographs are lower hemisphere. Darkened quarters represent compression (polarity Up) and white quarters represent dilatation (polarity Down). From the epicenter distribution, four clusters were selected to make a composite focal mechanism analysis. There is too much ambiguity to define the focal mechanism for most individual events due to the small number of effective stations for one aftershock. Figure 9 gives the four composite focal mechanisms corresponding to events in each square. A majority of events in a same square display a consistent focal mechanism with each other. The larger stereo graphs in figure 9 represent such predominant focal mechanism for their corresponding clusters. There are a small number of events in each cluster which can not be interpreted in the predominant focal mechanism. They are drawn separately to match their different mechanism, using smaller stereo balls. This deviation of focal mechanism is likely related to the complexity of faults in the area.

From the four predominant focal mechanism obtained, several features could be noticed. First of all they all fundamentally present normal faulting with very small strike slip component. Rake angles are larger than 75 degree from horizontal (less than 15 degree strike slipping component). Second, there is a small rotation of the T axis (Tension axis), toward a more north-south

direction at the northern end of the aftershock zone. In our result the T axis rotates from 130° at south to near 155° at north (T axis angle is measured clockwise from due north direction).

Both the findings are supported by geological observations. Detailed pre- and post-earthquake field measurement had indicated the earthquake was a normal faulting. In addition a young terrace found right along the shore line might imply a northeast-southwest trending normal fault existing at the foot of terrace and parallel to the shore line [G. King: pers. comm. 1989]. This would be an active normal fault and downthrown seaward. It contributed to the formation of the terrace. If this is true the northern part of Whakatane graben would have some more extensional component in the north-south direction. Rotation of the T-axis in our aftershock focal mechanisms would be consistent with such a tendency. terrace age was estimated at about 1,000 years and if the terrace is 10 m standing out from its foot the slip rate of the new fault would be on the order of 1 cm/year. The T axis direction geologically measured had a general agreement with our average result [Crook and Hannah 1989, Walcott 1984, Beanland at al 1989].

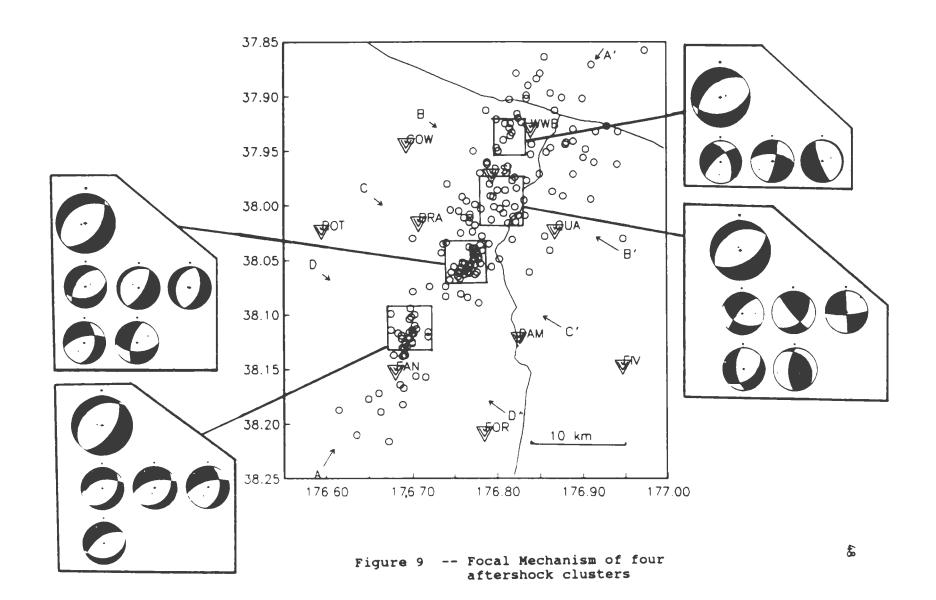
The percentage of events within the southern square which compose the predominant focal mechanism is somewhat higher than that in the northern square. Together with the characteristics of a more scattered epicenter distribution in the north it implies the faulting during the 1987 earthquake is more complicated in the north than in the south, where possibly only one single fault was involved in the earthquake. But in the north perhaps more small

faults were involved during the faulting process of the main shock. In any case it appears that the diffuse distribution of aftershocks can only be consistent with activation of numerous small faults in the aftershock sequence. The numerous known or unknown active faults in Whakatane graben provided much possibility in the process.

Geological observations after the 1987 Edgecumbe earthquake made by Beanland at al [Beanland at al 1989] suggested the dip of the Edgecumbe fault which was the major rupture fault in the earthquake is probably 55°. Actually all available results from gravity analysis, seismic study and drillhole samples about dip angles of faults within the graben seem that they are not less than 35°. They are estimated around 45-55° [Anderson & Webb 1989, Nairn & Beanland 1989, Woodward 1989]. Most of surface ruptures in relatively northern part of the rupture zone were observed downthrown to northwest. So fault planes in the top three major stereo balls should be the northwest dipping nodal planes. In such a way, their dip angles are about 40-55°, agreeing with observations. But in the bottom stereo ball if the northwest dipping nodal plane is interpreted as fault plane its dip angle is only 30°, which is too small compared to the various results above. The cross section in figure 5d which corresponds to the same cluster of aftershocks also is more consistent with a steeply dipping fault downthrown to the southeast than with a shallowdipping fault plane downthrown to the northwest, although that clue is weak. Thus the corresponding focal mechanism could be explained

that the southeast-dipping nodal plane is the fault plane which now is downthrown to southeast and has a dip angle 55°. In field observation there are surface breaks in the relatively southern part of the rupture zone which were indeed found downthrown to southeast (Rotoitipakau faults, Fig. 1). Those Rotoitipakau fault surface ruptures are located northwest of Mt. Edgecumbe while the southern aftershock cluster is located southeast to the Mt. Edgecumbe. Extrapolation of those surface ruptures, however, allow the possibility that maybe the Rotoitipakau fault or related southeast dipping fault, extend more underneath to the south. If so, they could more reasonably on geometry contribute to the aftershocks in the southern one cluster. Another suggestion is of course also possible to explain the southeast downthrown focal mechanism: different faults having no surface breaks under the southern cluster location may also be the source of those aftershocks. The data has not had any certain answer to this problem.

With the fault planes so determined the strike direction shown by the four major stereo balls is ranging from 40 to 70 degree northeast. The surface rupture observations are consistent with this.



## CONCLUSION

Aftershocks showed again that the 1987 Edgecumbe earthquake was a shallow normal faulting earthquake with a small (15 degree on average) strike slip component. Predominant focal mechanism presented the faulting with average N50°E strike, and 50° dip to the northwest for northe a part and 55° dip to southeast for the southern part of the aftershock zone. Aftershock epicenter distribution scattered at least to 15 km wide area and focal mechanism displayed more complicated property in the northern part of the aftershock zone, probably caused by more small active faults than we thought involved in the 1987 Edgecumbe earthquake main shock faulting process. The southern part of the aftershock zone is relatively more simple. There aftershocks concentrated in an area only 7 km wide and focal mechanisms showed relatively more identity. It means probably only one single fault contributed to the aftershocks there, which as revealed is also a normal fault but dipping into southeast. Extensional axis has more north-south component on the zone close to the sea shore.

An aftershock epicenter distribution gap is present under Mt. Edgecumbe, and might becaused by very high heat flow near Mt. Edgecumbe.

Overall our study of later aftershocks of the 1987 Edgecumbe earthquake has provided new evidences which generally are consistent with the geological observations in that region. The

earthquake was the continuation of the process of Whakatane graben subsiding and extending.

It should be said that all of our results are not surprising for that extensional back arc graben with thin crust, high heat flow and active recent volcanic activity.

## REFERENCES

- Anderson, H. and T. Webb, "The Rupture Process of the Edgecumbe Earthquake, New Zealand", New Zealand Journal of Geology & Geophysics, Vol.32, No.1, 1989, pp.43-52.
- Beanland, S., Kevin R. Berryman and Graeme H. Blick, "Geological Investigations of the 1987 Edgecumbe Earthquake, New Zealand",

  New Zealand Journal of Geology & Geophysics, Vol.32, No.1,

  1989, pp.73-92.
- Cole, J. W. (1979), "Structure, Petrology and genesis of Cenozoic Volcanism, Taupo Volcanic Zone, New Zealand--A Review.", New Zealand Journal of Geology & Geophysics, Vol.22, pp.631-657.
- Crook, C. N. and J. Hannah, "Regional Horizontal deformation

  Associated with the 1987 Edgecumbe Earthquake, Bay of Plenty,

  New Zealand An Introduction", New Zealand Journal of Geology

  & Geophysics, Vol.32, No.1, 1989, pp.93-98.
- Crosson, R. S. (1976), "Crustal Structure and Modelling of Earthquake data,1: Simultaneous Least Squares Estimation of Hypocenters and Velocity Parameters.", J. Geophys. Res., Vol. 81, pp3036-3046.
- Hanks, T. C. and Kanamori, H. (1979), "A Moment magnitude Scale",

  J. Geophys. Res., Vol.84, pp2348-2350.
- Jackson, J. A. (1987), "Active Normal Faulting and Crustal Extension", in: Croward, M.P., Dewey, J.F. and Hancock, P.L. ed. Continental Extension Tectonics. Geological Society

- special publication, Vol.28, pp.3-17.
- Klein, F. W. (1978), "Hypocenter Location Program: HYPOINVERSE", <u>US</u>

  <u>Geological Survey Open File 78-694.</u>
- Nairn, I. A. (1976), "Late Quaternary Faulting in the Taupo Volcanic Zone.", in Nathan, S. ed. <u>Comp. Excursion Guide</u>, No. 55A and 55C, 25th International Geological Congress.
- Nairn, I. A. and Sarah Beanland (1989), "Geological Setting of the 1987 Edgecumbe Earthquake, New Zealand", New Zealand Journal of Geology & Geophysics, Vol.32, No.1, 1989, pp.1-14.
- Robinson, R., "Aftershocks of the 1987 Edgecumbe Earthquake, New Zealand: Seismological Structural Studies Using Portable Seismographs in the Epicenter region", New Zealand Journal of Geology # Geophysics, Vol.32, No.1, 1989, pp.61-72.
- Priestley, Keith (1989), "Source Parameters of the 1987 Edgecumbe Earthquake, New Zealand", New Zealand Journal of Geology-& Geophysics, Vol.32, No.1, 1989, pp.53-60.
- Staff of New Zealand Department of Scientific and Industrial Research (1987), "The 1987 March 2 Earthquake near Edgecumbe, North Island, New Zealand", EOS Transactions of the American Geophysical Union, Vol.68, pp.1162-1171.
- Studt, F. E. and Thompson, G. E. K. (1969), "Geothermal Heat Flow in the North Island of New Zealand.", New Zealand Journal of Geology & Geophysics, Vol.12, pp.673-683.
- Stern, T. A. (1985), "A Back-Arc Basin Formed within Continental Lithosphere: The Central Volcanic Region of New Zealand.",

  Tectonophysics, Vol.112, pp.385-409.

- Walcott, R. I. (1984), "The Kinematics of the Plate Boundary Zone through NewZealand: A Comparison of Short- and Long-Term Deformations", Geophysical Journal of Royal Astronomical Society, Vol.79, pp.613-633.
- Woodward, D. J., "Geological Structure of the Rangitaiki Plains
  near Edgecumbe, Nea Zealand, from Seismic Data", New Zealand

  Journal of Geology & Geophysics, Vol.32, No.1, 1989, pp.15
  16.